

Monolithic High-Speed Pin Driver

### **Features**

- Wide ±12V output levels
- 250 ps dispersion
- 3 ns delay times
- 1V/ns slew rate—adjustable
- Low overshoot and aberrations in  $50\Omega$  systems
- 3-state output
- Power-down mode reduces output leakage to nanoamperes
- Overcurrent sense flag available to protect internal output devices
- Buffered analog inputs
- Differential logic inputs are compatible with ECL, TTL, and CMOS

### **Applications**

- Memory testers
- ASIC testers
- Functional board testers
- Analog/digital incoming component verifiers
- Logic emulators

### **Ordering Information**

Part No.	Temp. Range	Package	Outline#
EL1056CM	0°C to +75°C	24-Lead	MDP0027
		Thermal SOL	
EL1056ACM	0°C to +75°C	24-Lead	MDP0027
		Thermal SOL	

### **General Description**

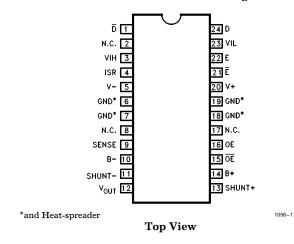
The EL1056 is designed to drive high-quality test signals into close or terminated loads. It has a dispersion of 250 ps or less — whether due to signal size or direction of edge. It can output a very wide 24V output span, encompassing all logic families as well as analog levels. The EL1056 is fabricated in Elantec's oxide isolated process, which eliminates the possibility of latch-up and provides a very durable circuit.

The output can be turned off in two ways; the OE pins allow the output to be put in a high-impedance state which makes the output look like a large resistance in parallel with 3 pF, even for back-driven signals with as much as  $2.5 \text{V}/\mu\text{s}$  slew rate. The E pins put the output in an even higher impedance state, guaranteed to 150 nA leakage in the EL1056A. This allows accurate measurements on the bus without disconnecting the EL1056 with a relay.

The EL1056 incorporates an output current sense which can warn the system controller that excessive output current is flowing. The trip point is set by two external resistors.

### **Connection Diagram**

### 24-Lead Thermal SOL Package



Note: All information contained in this data sheet has been carefully checked and is believed to be accurate as of the date of publication; however, this data sheet cannot be a "controlled document". Current revisions, if any, to these specifications are maintained at the factory and are available upon your request. We recommend checking the revision level before finalization of your design documentation.

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# EL1056A C/EL1056C

# Monolithic High-Speed Pin Driver

# Absolute Maximum Ratings ( $T_A = 25$ °C)

$v_s$	Voltage between V+ and V-	+33 <b>V</b>	$E, \overline{E}$	Input Voltages	V- to $V+$ or
v-	Supply Voltage	-18V			±6V Differential
B+	Supply Voltage	$ m V_{INH}$ to $ m V+$	Sense	Output Voltage	V- to $V+$
B-	Supply Voltage	$V-$ to $V_{ m INL}$	$V_{INH}$	Input Voltage	$V_{INI}$ = 0.3V to B+
$I_{SR}$	Input Current	0 mA to 3 mA	V <sub>INL</sub>	Input Voltage	B- to V <sub>INH</sub> +0.3V
$V_{SR}$	Input Voltage,		I <sub>OUT</sub>	Output Current	-60  mA to  +60  mA
	Power-Down Mode	-0.3V to $+6V$	$T_{I}$	Junction Temperature	150°C
Shunt+	Input Voltage	(B+) -5V to $B+$	$\tau_{\mathrm{A}}$	Operating Ambient Temperature	
Shunt-	Input Voltage	B - to (B -) + 5V	- A		-0°C to +75°C
Data, Data	Input Voltages	V- to $V+$ or		Range	
,		±6V Differential	$T_{ST}$	Storage Temperature	-65°C to +150°C
			$P_{\mathrm{D}}$	Power Dissipation ( $T_{\Delta} = 25^{\circ}C$ )	
OE, OE	Input Voltages	V- to $V+$ or	<b>-</b> D	,	
		$\pm6V$ Differential		(See Curves)	3.1W

### Important Note

All parameters having Min/Max specifications are guaranteed. The Test Level column indicates the specific device testing actually performed during production and Quality inspection. Elantec performs most electrical tests using modern high-speed automatic test equipment, specifically the LTX77 Series system. Unless otherwise noted, all tests are pulsed tests, therefore  $T_J = T_C = T_A$ .

Test Level	Test Procedure
I	100% production tested and QA sample tested per QA test plan QCX0002.
II	$100\%$ production tested at $ m T_A=25^{\circ}C$ and QA sample tested at $ m T_A=25^{\circ}C$ ,
	$ m T_{MAX}$ and $ m T_{MIN}$ per QA test plan QCX0002.
III	QA sample tested per QA test plan QCX0002.
IV	Parameter is guaranteed (but not tested) by Design and Characterization Data.
v	Parameter is typical value at $ m T_A=25^{\circ}C$ for information purposes only.

### **DC Electrical Characteristics**

 $T_A = 25^{\circ}C$ ,  $V_{+} = B_{+} = 15V$ ,  $V_{-} = B_{-} = -10V$ ,  $R_{SHUNT+} = R_{SHUNT-} = 6.5\Omega$ , no load. Data, E, and OE from -1.6V to -0.8V.  $I_{SR} = 800~\mu$ A.  $V_{INH} = 5V$ ,  $V_{INL} = -1.6V$ 

Parameter	Description	Min	Тур	Max	Test Level	Units
I <sub>S</sub>	(V+)+(B+),(V-)+(B-) Supply Currents		52	60	I	mA
I <sub>S</sub> , dis	(V+)+(B+),(V-)+(B-) Supply Currents, Disabled		17	25	I	mA
I <sub>VINH</sub>		-20	-3	20	I	μΑ
I <sub>VINL</sub>		-20	2	20	I	μΑ
I <sub>DATA</sub>		-30	-15	30	I	μΑ
$I_{OE}$	OE Input Current	-30	-14	30	I	μΑ
$I_{ m E}$	E Input Current	-20	7	20	I	μΑ
$V_{SR}$	Voltage at I <sub>SR</sub> Pin	0	20	40	I	mV
$I_{SHUNT+}, I_{SHUNT-}$			4	7	I	mA
$V_{SHUNT+}, V_{SHUNT-}$	Sense Threshold at Shunts	160	200	250	I	mV
I <sub>SENSE</sub>	Sense Output Currents	1	1.5	2	I	mA
V <sub>OS</sub>	Output Offset, Data High, $V_{INH}=0V$ , $V_{INL}=-1.6V$ Data Low, $V_{INL}=0V$ , $V_{INH}=5V$	-50 -100		50 100	I I	mV mV

Monolithic High-Speed Pin Driver

### DC Electrical Characteristics — Contd.

 $T_{A} = 25^{\circ}\text{C, V} + = B + = 15\text{V, V} - = B - = -10\text{V, } \\ R_{SHUNT+} = R_{SHUNT-} = 6.5\Omega, \text{ no load. Data, E, and OE from } -1.6\text{V to } -0.8\text{V. } \\ I_{SR} = 800 \ \mu\text{A. V}_{INH} = 5\text{V, V}_{INL} = -1.6\text{V}$ 

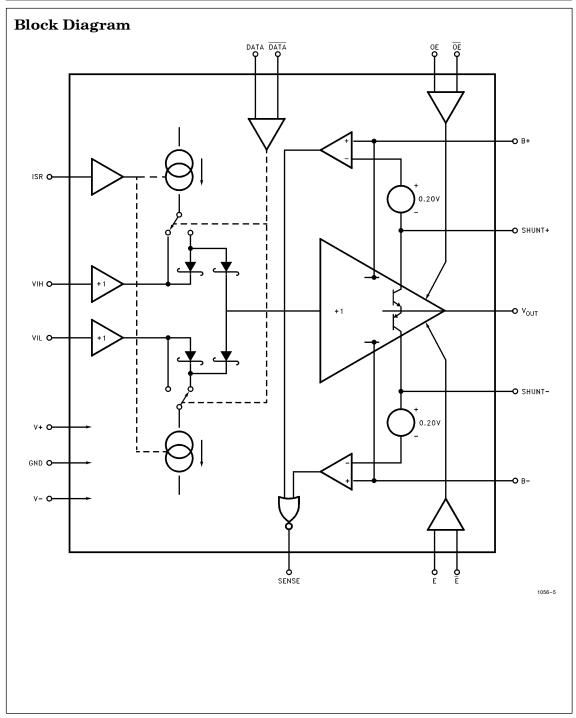
Parameter	Description	Min	Тур	Max	Test Level	Units
Eg	Gain Error Data High, $V_{INH}$ from 0V to 5V, $V_{INL}=-1.6$ V, No Load Data Low, $V_{INH}=5$ V, $V_{INL}$ from $-5$ V to 0V, No Load	-1.5 -1.5	-0.6 -0.6	0 0	I I	% %
NL	Gain Nonlinearity Data High, $V_{INH}$ from 0V to 10V, $V_{INL}=-1.6$ V, No Load Data Low, $V_{INH}=5$ V, $V_{INL}$ from $-10$ V to 0V, No Load		0.04 0.06		v v	% %
PSRR	Power Supply Rejection Ratio of $V_{OUT}$ with Respect to $B+$ , $B-$ , Shunt+, or Shunt- Potential		2.2		v	mV/V
R <sub>o</sub> , en	Output Resistance, Enabled, Il $=\pm 20$ mA	4.5	6	7.5	I	Ω
R <sub>o</sub> , dis	Output Resistance, Output Disabled, $V_O = -1.6V$ to $-5V$ , EL1056C EL1056AC	20K 100K	100K 200K		I	Ω
I <sub>o</sub> , dis	Output Current, Output, Disabled, V <sub>O</sub> = 0V	-20	5	20	I	μΑ
I <sub>o</sub> , off	Output Leakage, E Low, (Shut-Down), V <sub>O</sub> = 0V, EL1056C EL1056AC	-20 -150		20 150	I I	μA nA

### **AC Electrical Characteristics**

 $T_A=25^{\circ}\text{C, V}+=B+=+15\text{V, V}-=B-=-10\text{V, } \\ R_{SHUNT+}=R_{SHUNT-}=6.5\Omega. \\ R_L=500\Omega. \\ 50\Omega+22 \text{ pF snubber included at output. Data E, and OE from } \\ -1.6\text{V to } \\ -0.8\text{V. I}_{SR}=800 \\ \mu\text{A. ECL swing is defined by } \\ V_{INH}=-0.8\text{V and V}_{INL}=-1.6\text{V. CMOS swing defined by V}_{INH}=5\text{V and V}_{INL}=0\text{V. Propagation delay is measured at } \\ 0.4\text{V movement of output.}$ 

Parameter	Description	Min	Тур	Max	Test Level	Units
$T_{\mathrm{PD}}$	Propagation Delay, CMOS Swing	1.0	3.0	4.5	I	ns
Dis	Propagation Delay Dispersion Due to Output Edge Direction From ECL to CMOS Swings Due to Repetition Rate		250 250 80	450 450	I I V	ps ps ps
SR	Output Slew Rate, CMOS Swing, 20%-80%	0.8	1	1.2	I	V/ns
SR <sub>sym</sub>	Slew Rate Symmetry		3	10	I	%
TR	Output Rise Time, ECL Swing, 20% –80%		2.2		v	ns
os	Output Overshoot CMOS Swing ECL Swing ( $I_{SR} = 350 \mu A$ )		190 65	500	I V	mV mV
$T_{ m dis}$	Output Disable Delay Time		4.7	6.5	I	ns
T <sub>en</sub>	Output Enable Delay Time		6.0	8.5	I	ns
C <sub>o</sub> , dis	Output Capacitance in Disable		3		v	pF
$T_{ m off}$	Power-Down Delay Time		0.5		v	μs
Ton	Power-On Delay Time		90		v	ns
C <sub>o</sub> , off	Output Capacitance in Power-Down		50		v	pF
T <sub>sense</sub>	Comparator Delay Time — Switching ON Switching Off		1.5 0.4		V V	μs μs

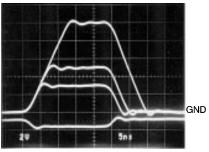
# EL1056AC/EL1056C Monolithic High-Speed Pin Driver



Monolithic High-Speed Pin Driver

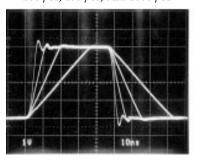
### **Typical Performance Curves**

# 10V, CMOS, TTL, and ECL Outputs into $550\Omega$ Load



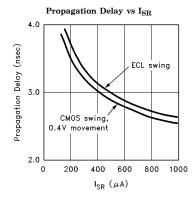
1056-6

# CMOS Output at $I_{SR}=100~\mu A$ , 200 $\mu A$ , 400 $\mu A$ , and 1000 $\mu A$



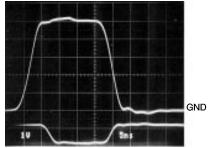
GND

1056-8



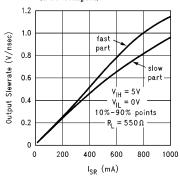
1056-10

### CMOS and ECL Outputs As Seen at the End of an Unterminated Cable, Backmatched at Driver



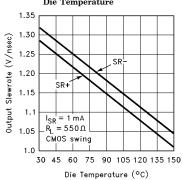
1056-7

# Output Slewrate vs $I_{SR}$ (Two Samples)



1056

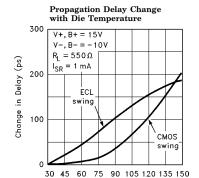
### Output Slewrate vs Die Temperature



1056-11

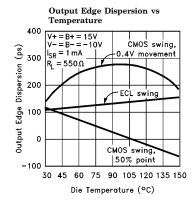
Monolithic High-Speed Pin Driver

### Typical Performance Curves - Contd.



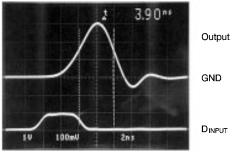
Die Temperature (°C)

1056-12



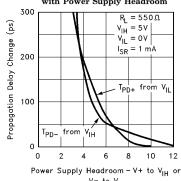
1056-14

### Minimum Output Pulse Width



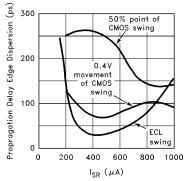
1056-16

# Change in Propagation Delay with Power Supply Headroom

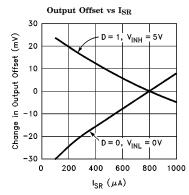


V- to V<sub>IL</sub>

### Edge Dispersion vs $I_{\rm SR}$



1056-15

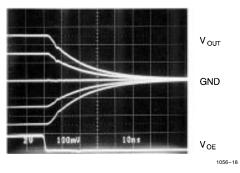


1056-17

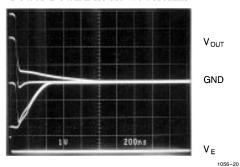
Monolithic High-Speed Pin Driver

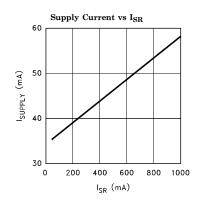
## ${\bf Typical\ Performance\ Curves-Contd}.$

### **Tristate Turn-off Waveforms**

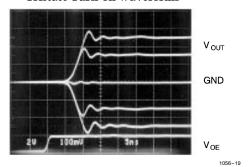


### **Power-Down Disable Waveforms**

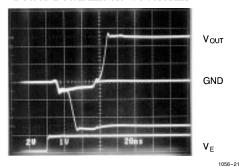




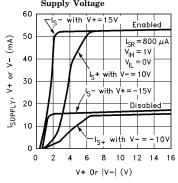
### **Tristate Turn-on Waveforms**



### Power-Down Enable Waveforms

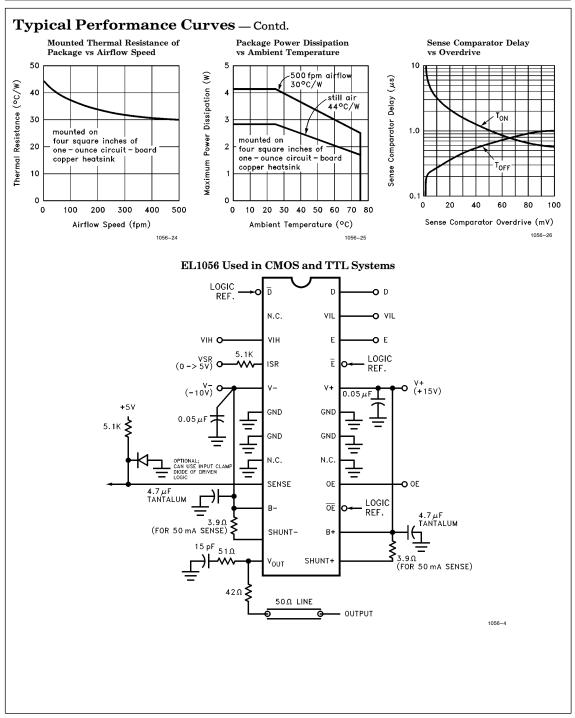






1056-22

# Monolithic High-Speed Pin Driver



Monolithic High-Speed Pin Driver

### **Applications Information**

### **Functional Description**

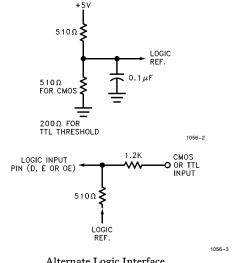
The EL1056 is a fully integrated pin driver for automatic test systems. Pin drivers are essentially pulse generators whose high and low levels can be externally programmed and accurately switched in time, as well as incorporating an output switch to disconnect the driver from a measurement bus. Additionally, the EL1056 has programmable slewrate.

### **Control Voltage Inputs**

The analog level inputs are named  $V_{\mbox{\scriptsize INH}}$  and V<sub>INL</sub>, and the output replicates them as controlled by logic inputs. The analog inputs are buffered and have bandwidths of 35 MHz and slewrates of 25V/µs. For full slewrate, 4V of headroom should be given to the inputs, that is  $V_{\mathrm{INH}}$  should be 4V less than V+ or B+, and  $V_{\mbox{\footnotesize{INL}}}$  should be 4V more positive than V- or B-. At lower slewrates ( $I_{SR} = 500 \mu A$  or less), 3V of headroom will suffice. Insufficient headroom causes distorted output waveforms or delay errors in output transitions. V<sub>INH</sub> may be lower in voltage than  $V_{\mbox{\scriptsize INL}}$ , but the output will not follow the control logic correctly. Furthermore, V<sub>INH</sub> should be 200 mV more positive than V<sub>INL</sub> (the minimum output amplitude) for accurate switching.

### **Logic Inputs**

The logic inputs are all differential types, with both NPN and PNP transistors connected to each terminal. They are optimized for differential ECL drive, which optimizes + to - edge delay time matching. Larger logic levels can introduce feedthrough glitches into the output waveform. For CMOS input logic levels, an ECL output waveform will show feedthrough when the input risetime is shorter than 8 ns, differential or single-ended. CMOS output swings show less aberration, and the EL1056 can tolerate a 4 ns single-ended risetime or 2 ns risetime for differential inputs. Attenuating CMOS or TTL inputs to 1 Vp-p will eliminate all logic feedthrough as shown in Figure 1.



Alternate Logic Interface Figure 1

### **Slewrate Control**

The slewrate is controlled by the  $I_{SR}$  input. This is a current input and scales the output slewrate by a nominal 1.25V/ns/mA. The slewrate maintains calibration and symmetry to at least as slow as 0.2V/ns. The practical upper end of  $I_{SR}$  is 1 mA, and supply current increases with increasing  $I_{SR}$ .

The  $I_{SR}$  control can be used to adjust individual pin drivers to a system standard, by adjusting the value of its series resistor. Slewrate can also be slowed to reduce output ringing and crosstalk.

With ECL output swings, there is not enough voltage excursion to incur slewrate delays to 50% logic threshold. The risetime, delays, and dispersions do not degrade with reasonably reduced  $I_{\rm SR}$ , and overshoot will reduce markedly. An  $I_{\rm SR}$  of 350  $\mu\rm A$  produces a very good ECL output, and driver dissipation is also reduced.

Monolithic High-Speed Pin Driver

### **Applications Information** — Contd.

The  $I_{SR}$  pin is connected to the emitter of a PNP transistor whose base is biased a diode below ground (see Figure 2). Thus, the  $I_{SR}$  input looks like a low impedance for positive input currents, and is biased close to ground. A protection diode absorbs negative currents, and the input PNP will not conduct. In power-down mode, the PNP releases its current sink and the external circuit must not present more than 6V to the disabled  $I_{SR}$  input, or emitter-base damage to the NPN will occur within the driver. A signal diode or zener can be used to clamp the  $I_{SR}$  input for positive input voltages if the voltage on the  $I_{SR}$  resistor is potentially greater than 6V when the driver is in power-down mode.

### **Output Stage-Tristate Mode**

In tristate mode (OE low) the output transistors have their emitter-base junctions reverse-biased by a diode voltage. This turn-off voltage is in fact provided by an internal buffer whose input is connected to the output pin (see Figure 3). Transistors Q1–Q4 form the output buffer in normal mode. The tristate mode buffer Q5–Q8 replicates externally impressed voltages from the output pin onto the internal schottky switch node. They also turn off Q1–Q4 by a reverse diode voltage between bases and emitters, effectively bootstrapping the internal voltages, so that no transistor's base-emitter junction is reverse-biased by

a damaging potential. Another benefit is that the capacitance seen at the output in tristate mode is reduced.

Because the tristate buffer's input is connected to the output terminal, the output is quite "alive" during tristate. For instance, the input bias current of the buffer is seen as the tristate "leakage", and its variation with applied voltage becomes tristate input impedance.

The tristate input current is like a current source, and it can drag an output to unpredictable voltages. It is not a danger to connect a tristated output that has drifted to, say, -6V to a logic pin of a device to be tested. The tristate output current will simply comply with whatever voltage the connected part normally establishes.

The tristate input impedance is also quite active over frequency. The output can oscillate when presented with resonant or inductive impedances. To prevent this, a snubber should be connected from output to ground, consisting of a resistor in series with a small capacitor. The snubber can also reduce the reflections of the coaxial line when driven from the far end, since the line appears to have an open termination during tristate. Typical values for the resistor are  $50\Omega$  to  $75\Omega$ , and 12 pF to 22 pF for the series capacitor. The effect of the snubber is to "de-Q" resonances at the output.

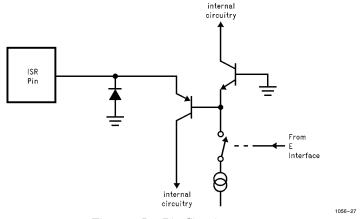


Figure 2. I<sub>SR</sub> Pin Circuitry

Monolithic High-Speed Pin Driver

# Applications Information — Contd. | Internal | Shunt+ | Other | Other

Figure 3. Output Stage Circuit in Tristate Mode

### **Output Stage-Normal Mode**

Capacitive loads can cause the output stage to ring. Little ringing occurs for loads less than 25 pF, but substantial ringing for more than 40 pF. Terminated transmission lines cause no ringing, and actually suppress it as a snubber does. A terminated line draws heavy DC current, however, and greatly raises dissipation.

Driving a back-terminated line also causes little ringing and does not cause DC dissipation. The series matching resistor between the EL1056 output and a back-terminated line also serves to isolate the driver from capacitive loads and short-circuits. The slewrate of the driver slows by about 10% when driving a  $50\Omega$  back-matched

line, as seen at the end of the line. The snubber can be on either side of the back-match resistor. When placed on the line side it creates a high-frequency termination for the line when the driver is tristated, but it slows the output small-signal risetime by about 10% (although not slew-rate). When placed on the driver side of the back-match resistor, no speed reduction occurs in normal mode but the cable is more poorly terminated in tristate.

The transient currents that occur when driving capacitive or back-matched loads can be very high, approaching 100 mA. The driver is capable of outputting a peak of 140 mA, but long-term

Monolithic High-Speed Pin Driver

### Applications Information — Contd.

load currents must be limited to 60 mA. Short-circuits can rapidly destroy the EL1056, although the part will survive for 20 ms periods. If there is the possibility of output load fault the overcurrent sense circuitry should be used to signal alarm to the controlling system, which should ultimately activate the tristate mode to relieve the output stage. Driving large static currents also raises internal dissipation and should be part of the thermal budget.

The collectors of the output transistors are connected to the Shunt terminals, and the output stage drivers' collectors are connected to the  $\rm B^+$  and  $\rm B^-$  terminals (see Figure 4). The Shunt lines can have transient currents as high as 120 mA and are separated from the V+ and V- terminals to keep switching noise out of the control and logic circuitry. A bypass capacitor should be connected to the B+ and B- terminals.

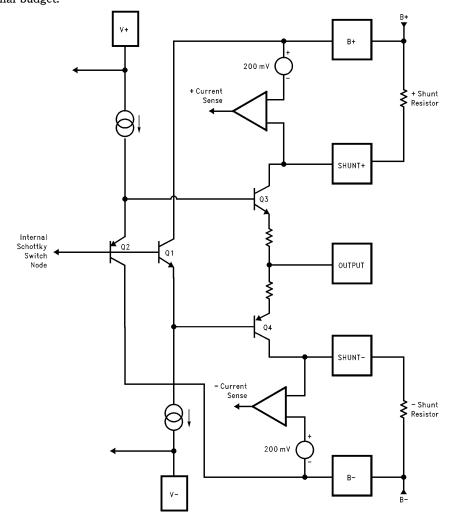


Figure 4. Output Stage in Normal Mode

Monolithic High-Speed Pin Driver

### Applications Information — Contd.

### **Overcurrent Protection**

The sense comparators are available to alert the test system's controller that the driver is outputting excessive current. Shunt resistors are connected from B+ to Shunt+ and B- to Shunt-. When the internal comparators sense more than a nominal 200 mV drop on the shunts, they cause a 1.5 mA current to be sunk from the Sense terminal. The comparators are of "slow attack, fast decay" design, so that transient load currents will not trigger a sense output; only a sustained overcurrent will.

The sense resistors must not be inductive, and the skin resistance of long, narrow connections between Shunt and B+ or B- can cause transient voltages that produce output overshoot (but not ringing).

The Sense output is simply a switched current source connected to V-. It can be used to interface to CMOS, TTL, or ECL inputs. For CMOS and TTL, it can be connected to a pull-up resistor to +5V of 10K value. This establishes a logic high value, and a clamp diode (internal to TTL) establishes a low level of -0.6V. For ECL, a gate should be available to provide a static logic high level. An  $820\Omega$  pull-up resistor is wired to that output. The logic low will be more negative than is usual for ECL, but this will cause no problem. In all cases, multiple Sense outputs may be connected together from many drivers to effect a wired-or function.

A further protection scheme is to provide a series resistor from B+ to V+ and B- to V-. The resistor serves to limit the output fault current by allowing B+ and B- voltages to sag under heavy load. This also reduces the dissipation on the output transistors for valid loads. Because

B+ and B- are separately bypassed, these voltages will sustain under transient loads and dynamics will not be affected.

### **Output Accuracy**

The accuracy of the output voltage depends on several factors. The first is the gain error from  $V_{\rm INH}$  or  $V_{\rm INL}$  to the output, unloaded. The gain error is nominally -0.6%, and has a few tenths of a percent variation between parts. The second is supply rejection. If the B+, B-, Shunt+, or Shunt- voltages are different from those used by Elantec to test the part, there will be about 2.2 mV systematic shift in output offset per volt of supply variation. The V+ and V- supplies have much less influence on output error. Finally, there is a random  $V_{\rm OS}$  error as specified in the data table.

Of course, the finite output impedance of the EL1056 will cause additional output error when the driver is loaded.

### Power-Down

The EL1056 incorporates a power-down feature that drastically reduces power consumption of an unused driver and also drops the output leakage current to nanoamperes ("A" grade only). The output is not a low capacitance in this mode, however, and transients driven from the cable can momentarily turn on the output transistors. Power-down is intended to allow the switching of accurate DC meters onto the bus without having to relay out the driver's leakage current. It takes about 40  $\mu s$  for the output leakage to sag to nanoamperes, but this is still much faster than relays or voltmeters.

Power-down is controlled by the E and  $\overline{E}$  differential inputs. There is no problem with logic amplitude or slewrate, and input resistor networks are not needed.

Monolithic High-Speed Pin Driver

### Power Down — Contd.

### Supply and Input Bypassing

The V+, B+, V-, and B- leads should be bypassed very closely with 0.1  $\mu F$  capacitors, preferably chip type. There should be a wide ground plane between bypasses, and this can be the heat-sink copper. It is wise to also have a 4.7  $\mu F$  tantalum bypass capacitor within a couple of inches to the driver.

The logic inputs are active device bases, and can oscillate if presented with inductive lines. A local resistor of  $1000\Omega$  or less to ground will suffice in de-Q'ing any resonance. A 100 pF or larger capacitor can also serve as a bypass.

### Thermal Considerations

The package of the EL1056 includes two fused leads on each side which are connected to the internal die mounting metal. Heat generated in the die flows through the mounting pad to the fused leads, and then to the circuit-board copper, achieving a thermal resistance to air around 40°/W. Characterization curves show the thermal resistance versus airflow rate. Consult the EL1056 Demonstration Board literature for a suggested board pattern. Note that thicker layers of copper than we used improves the thermal resistance further, to a limit of 22°C/W for an "infinite heatsink" directly soldered to the fused leads.

As a practical limit, the die temperature should be kept to 125°C rather than the allowable 150°C to retain optimum timing accuracies.

Monolithic High-Speed Pin Driver

### General Disclaimer

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